

1 Lifecycle cost and CO₂ emissions of residential heat and electricity prosumers in
2 Finland and the Netherlands

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14

15 **Abstract**

16 The complexity of finding solutions to reach energy sustainability in the built environment poses a
17 significant challenge. Therefore, there is interest in adequate management of the generation, conversion,
18 storage, use and exchange of heat and electricity. The novelty of this study exists in presenting and
19 comparing multiobjective optimizations for operational CO₂ emissions and lifecycle costs (LCC) of heat
20 and electricity prosumers in the Netherlands and Finland, with and without net-metering. The premise relies
21 on using surplus electricity to drive heat pumps for heat export instead of exporting surplus electricity. In
22 the Netherlands, the calculated cost optimal solutions consist of using surplus electricity to drive an air
23 source heat pump and export heat, with CO₂ emissions and Δ LCC of -41.1 kgCO₂eq/(m² a) and €69.7/m²
24 (22% lower), respectively. In Finland, the heat export strategy allows a Δ LCC of €-24.5/m² (8% lower),
25 with CO₂ emissions reduced by -32.5 kgCO₂eq/(m² a). Without net-metering, the Δ LCC of the energy
26 system rises to €4/m² in the Netherlands; with net metering, the Δ LCC lowers to €65.6/m² in Finland. The
27 results indicate the potential for significant economic and emission reductions in heat and electricity
28 prosumers.

29 **Keywords:** CO₂ emissions, LCC, heat and electricity prosumers, multiobjective optimization, renewable
30 energy systems

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Abbreviations

ASHP	Air source heat pump
DH	District heating
DHW	Domestic hot water
FH	Floor heating
GSHP	Ground source heat pump
HWST	Hot water storage tank
LCC	Lifecycle cost
NG	Natural gas
NPV	Net present value
NSGA-II	Non-dominated Sorting Genetic Algorithm II
NZEB	Net-zero energy building
O&M	Operation and maintenance
PE	Primary energy
PV	Photovoltaic
ST	Solar thermal
VAT	Value added tax
WT	Wind turbine
WP	Wood pellet

33

Symbols

A_{net}	Net conditioned area
A_{salv}	Salvage value
C	Expense
$CO_{2,eq}$	Equivalent CO ₂ emissions
exp	Export
E	Energy
El	Electricity
F_1, F_2	Objective functions
F	Fuel
f_{CO_2}	Specific emissions factor
I_{ini}	Initial investment
imp	Import
net	Net
$single$	Single
th	Thermal
Q	Heat
X	Exergy
x	Continuous design variable
y	Discrete design variable

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35

36 **1. Introduction**

37 Through the Energy Performance of Building Directive (EPBD), all Member States of the European Union
38 agreed to find and implement solutions to reach energy sustainability in the built environment [1]. This has
39 sparked a vast amount of discussion and research in the countries involved, as each of them has its own
40 socio-economical, cultural and environmental context, and thus each of them needs to find its own most
41 suitable solution(s). This is seen in the varying building energy standards or references defined by each
42 country, such as the Energy Saving Ordinance in Germany [2], the Nearly Energy Neutral Buildings
43 (BENG) in the Netherlands [3], the French Thermal Regulation [4] and the National Building Code of
44 Finland [5].

45 A topic that faces a high level of complexity is the interaction between the different forms of energy
46 generated onsite and the energy demand of the building, which in turn influence the unidirectional and
47 bidirectional exchanges between the building and the grid(s) [6]. Georges et al. [7] investigated the potential
48 to improve the balance between onsite generation and demand. They found that load management and
49 optimal sizing of photovoltaics (PV) systems enhanced load matching, cost savings and CO₂ emission
50 reductions. Brange et al. [8] studied heat prosumers in Sweden and showed their potential to contribute
51 significant amounts of heat to district heating grids, *heat prosumers* being buildings that generate a surplus
52 of heat and export it beyond the system boundaries. Salom et al. [6] discuss indicators that aim to measure
53 the interaction between generation, demand and grid, such as *load matching* or *grid interaction*. The authors
54 highlight on the need to identify appropriate values for each of these indicators based on the type of
55 building, the climate, and the energy type. Even though a net-zero energy building is commonly thought to
56 be a building where the annual electricity consumption is equal to its annual electricity generation [9],
57 buildings hardly rely on only one form of energy. Thus, Cao et al. [10, 11] identified the need for
58 differentiating between electricity, heating and cooling, and developed and tested separate indicators for
59 each. Their study shows the complexity of evaluating the performance of a system that includes energy grid
60 connections, generation and storage components for different forms of energy. Moreover, in the definition
61 of the 4th Generation District Heating, Lund et al. [12] contemplate smart interaction between the grid and
62 the fluctuating energy sources, such as PV systems or wind power, and they warn that grid interaction with
63 low-energy buildings is a major challenge since low-temperature sources and heat recycling might be
64 required. Therefore, there is interest in adequate management of the generation, conversion, storage, use
65 and exchange of various forms of energy in the built environment; failing to do so might leave the optimal
66 solutions out of reach.

67 The complexity of this problem poses a significant challenge to the scientific community across Europe,
68 since building topology, insulation levels, climate, energy supply and demand, prices, regulatory

69 frameworks, and several other conditions must be addressed to evaluate the building performance. Single
70 or multiobjective optimization can assist in this endeavor since it allows identifying optimal solutions when
71 several variables are present. Multiobjective optimization enabled Mohamed et al. [13] to evaluate system
72 configurations for small-scale multigeneration technologies in zero-energy buildings. The authors
73 identified the optimal solutions in terms of cost and environmental benefits, as well as the effect of including
74 PV panels in the system. The mixed integer linear programming approach by Harb et al. [14] showed that
75 the optimal design and operation strategy of energy systems depends on the type of residential building. In
76 their study, they found that boilers in combination with PV are preferable for single-family houses, while
77 combined heat and power (CHP) and local heating networks are preferable for larger buildings and
78 neighborhoods, respectively. Hamdy et al. [15] conducted a multi-stage optimization process to find the
79 optimal combinations of building envelope and heat recovery options, and the corresponding optimal
80 heating/cooling systems. Through this process, the authors found that fulfilling and surpassing the current
81 energy standards in Finland can be achieved in a cost-optimal way, yet incentives are required get close to
82 the net-zero energy level. While these are only a few examples of optimization studies on energy system
83 design and/or management in the built environment, they illustrate the level of problem complexity that
84 this method can handle and the quality of the information it can provide.

85 The reported literature gives an insight into the applicability of optimization in the study of the built
86 environment, and into the challenge of optimal design and management of onsite energy systems. Thus, it
87 is apparent that optimization can allow finding the energy solutions in buildings that deliver the best
88 performance. Further, investigating heat and electricity, as opposed to simply *energy*, presents alternatives
89 to how buildings can manage their onsite generation, and how they can exchange energy with its
90 surroundings. As a result, multiobjective optimization of onsite heat and electricity systems in the buildings
91 arises as an opportunity to come closer to sustainability in the built environment. This was investigated by
92 Manrique Delgado et al. [17], where optimized energy systems for heat and electricity prosumers in Finland
93 were presented. The study focuses on the environmental, economic and exergetic performance of a
94 residential building with several energy configurations. Among them, an option to use a ground source heat
95 pump (GSHP) to convert surplus electricity into heat for further export was presented and compared to
96 other traditional heat supply options such as CHP and district heating. The results show that the heat export
97 strategy can lead to optimal solutions concerning operational CO₂ emissions and lifecycle costs, yet the
98 most cost-optimal solution is reached with a more conventional GSHP system without heat export
99 capability. Overall, the results indicate potential and encourage further investigation of heat and electricity
100 prosumers, particularly regarding their performances under various economical, climatic and energetic
101 contexts.

102 The current study investigates the developed methodology [17] for its suitability in different conditions (the
103 Netherlands) in order to evaluate the generic nature of the methodology. For this purpose, multiobjective
104 optimizations for operational CO₂ emissions and lifecycle costs (LCC) of heat and electricity prosumers in
105 the Netherlands and Finland. It relies on using surplus electricity to drive heat pumps with the purpose of
106 exporting heat, instead of exporting the surplus electricity. While this aspect has been presented and
107 investigated previously [17, 18, 19], the topic remains far from exhausted. The novelty of this article relies
108 on four cornerstones. First, it presents the economic and emissions performance of heat and electricity
109 prosumers in the Netherlands and describes the optimal energy system configurations. Second, the study
110 presents the similarities, contrasts and transferable conclusions between prosumers in Netherlands and
111 Finland. This provides an insight into the performance of the energy systems in two different contexts where
112 climate, building typology, economic parameters, and energy practices are different. Third, the presence
113 and capacity of the generation and storage components along the optimal fronts is studied in detail, and
114 guidance on how to prioritize investments is given. Fourth, the article investigates the consequences for
115 heat and electricity prosumers, and for regular prosumers, of a possible phase-out of net-metering in the
116 Netherlands—which could lead to a poorer economic performance—and whether investments on energy
117 components should be prioritized differently. Additionally, this study serves to reassert the potential of the
118 heat export method by investigating its results under circumstances different from those in previous articles.

119 **2. Description of the Dutch and Finnish contexts**

120 This section presents the main characteristics of the Dutch and Finnish cases. The aim of the study is to
121 address typical single-family households in the Netherlands and Finland adhering to the respective
122 regulations. Further, cases with and without net-metering are studied for both countries, with the aim to test
123 the system performance under current and hypothetical conditions. For instance, while district heating
124 systems are not very common in the Netherlands, they are being encouraged [3]. In addition, a subcase is
125 presented where CO₂ and initial investment are optimized. For detailed data, such as initial investments,
126 O&M expenses and connection costs, please refer to Appendix A.

127 **2.1. Buildings**

128 The selected buildings adhere to strict building regulation frameworks in the Netherlands and Finland;
129 Table 1 shows several of their features. In the Netherlands, the building is a semi-detached terraced house,
130 which is a typical Dutch residential house [21, 3], representing about 40% of Dutch households [22]. The
131 building is based on the BENG (Nearly Zero Energy Building) reference building by the Netherlands
132 Enterprise Agency (RVO) [3]. A detailed description and the layout of the three-storey building can be
133 found in Kotireddy et al. [23]. The Finnish building is based on Villa ISOVER, a pilot project between the
134 two companies ISOVER and Fortum on the incorporation of onsite generation components in a highly-

135 insulated single-family house. It is a detached two-storey building that adheres to and exceeds the
136 regulations in Decree D3 of the National Building Code of Finland [5]. Further information about Villa
137 ISOVER is available in [25, 26]. The simulation model for Villa ISOVER was calibrated and validated
138 based on measured data from the building [18], with errors between the simulated and measured data of
139 roughly 5% and 3% for energy demand and supply, respectively.

140 **Table 1** – *Features of the buildings modelled for the Dutch and Finnish cases.*
141

142 **2.2. Heat supply options**

143 The studied Dutch heat supply systems consist of natural gas (NG) boilers—around 97% of residential
144 houses in the Netherlands use gas-based boilers [27]—and air source heat pumps (ASHP) with and without
145 heat export, whereas in Finland, the options are wood pellet (WP) boilers, and GSHP with and without
146 export. Boilers cannot be operated with electricity, and thus offer no potential to convert surplus electricity
147 into heat for further export. Heat pumps offer this possibility, and they are also common in both countries.
148 Also, they produce several units of heat per unit of consumed electricity, and therefore they are attractive
149 for the purpose of this study. Currently, due to local weather and ground conditions, ASHPs are more
150 preferred in Netherlands [28], while GSHPs have been suggested as optimal solutions for single-family
151 buildings in Finland [29]. All heat supply options are assumed to include a hot water storage tank (HWST)
152 with a capacity of 750 liters

153 **2.3. Economic aspects**

154 The energy prices depend on the energy carrier, the case study and the country. The Netherlands has
155 implemented support mechanisms for residential onsite generation technologies, such as net-metering and
156 tax deductions. Net-metering allow users to import and export energy from and to the grid whenever
157 required, ideally at the same price. There is a limitation in the Netherlands: if annual export exceeds the
158 annual import, the surplus is paid at a lower rate. It is uncertain whether this support scheme will continue
159 beyond 2020 [30, 31]. Finland has not implemented net-metering; the import price includes the spot market
160 price in NordPool [32] plus an energy tax and a transmission fee, and the export price consists only of the
161 spot market price minus a commission fee. Table 2 shows the electricity import and export prices and feed-
162 in tariff rates of the net-metering scenarios for both countries. The prices without net-metering in the
163 Netherlands and the prices with net-metering in Finland are assumptions based on the current price scheme
164 in each country. For the Netherlands, in the case of net-metering termination, the lower feed-in tariff rates
165 of the net-metering scenario are used for exported electricity irrespective of the annual energy balance. In
166 Finland, the import and export electricity prices with net-metering are assumed to be equal to the respective
167 average prices in 2015.

168 Regarding the price of exported heat, assumptions have been made for both countries, as such strategy has
169 been implemented to a very limited extent. An example is the open district heating grid in Stockholm, one
170 of the few existing grids that supports the heat export strategy [35]. In the Netherlands, the price is assumed
171 to be 40% of the operational energy cost of heat from an NG boiler. That is, the price of NG divided by the
172 boiler efficiency. In Finland, the price is assumed to be 40% of the price of heat from a district heating grid;
173 these price assumptions are comparable with the prices in the open district heating grid in Stockholm. The
174 heat export prices in the Netherlands and Finland at the beginning of the simulation amount to €0.034/kWh
175 and €0.038/kWh, respectively.

176 **Table 2** – *The electricity import and export prices with and without net-metering in the Netherlands and*
177 *Finland [33, 34, 32] in euro cents per kWh. The annual balance is positive if the exported electricity is*
178 *larger than the imported electricity, and vice versa.*

179 The electricity price escalation rates in the Netherlands and Finland are 1% and 4%, respectively, calculated
180 based on the nominal historical prices as shown in Figure 1. These prices correspond to the average values
181 for each year, unadjusted for inflation or else. The price of NG in the Netherlands and the price of wood
182 pellets (WP) in Finland remain constant throughout the year, starting at €0.077/kWh and €0.058/kWh,
183 respectively, with price escalation rates of 1% and 3.5%, respectively. The interest rate is set at 3% in both
184 countries.

185 Further support schemes are available in both countries. In the Netherlands, the VAT on the acquisition of
186 photovoltaic (PV) systems is returned. In Finland, a 45% tax deduction can be applied for on the installation
187 costs of PV and wind turbine (WT) systems [38].

188 **Figure 1** – *The nominal historical prices and price trends for various energy carriers for detached*
189 *houses in the Netherlands [36] and Finland [34, 37]. (El.: electricity; NG: natural gas; WP: wood pellets;*
190 *NL: Netherlands; FI: Finland)*

191 **2.4. Emission factors**

192 The specific emission factors in the Netherlands and Finland for the energy carriers are shown in Table 3.
193 Exported energy is assumed to replace energy production by the utilities, and thus there is no distinction
194 between factors for the import and export of electricity. It is also assumed that the generation from PV, WT
195 and solar thermal (ST) collectors has no operational emissions. Regarding heat export, in the Netherlands,
196 it is assumed to have an emission factor of 220.3 kgCO₂eq/MWh (replacing heat supplied by an NG boiler).
197 In Finland, heat export is assumed to replace import from a district heating grid, with an emission factor of
198 245 kgCO₂eq/MWh [39].

199 **Table 3** – *The specific emission factors f_{CO_2} in kgCO₂eq/MWh for the energy carriers in the Netherlands*
 200 *and Finland used in this study.*

201

202 **3. Research method**

203 In this section, the definition of the optimization problem and the approached method are presented. This
 204 includes the optimization problem itself, the mathematical expressions used to calculate the objective
 205 functions, the design variables, the simulation environment, and the multiobjective optimization tool and
 206 algorithm.

207 **3.1. The optimization problem**

208 The optimization problem in each case study is defined as

$$\text{Min } \{F_1(\mathbf{x}, \mathbf{y}), F_2(\mathbf{x}, \mathbf{y})\} \quad (1)$$

209 where

$$\mathbf{x} = (x_{PV}, x_{WT}, x_{ST}, x_{Battery})^T \text{ and } \mathbf{y} = (y_{STConn}, y_{HeatSys})^T \quad (2)$$

210 where F_1 and F_2 are the objective functions, vector \mathbf{x} contains the continuous design variables and vector \mathbf{y}
 211 contains the discrete design variables. The problems are unconstrained. Each decision variable (for a
 212 detailed description, see Table 4 and Table 5) represents (i) the installed capacity of the system components,
 213 $x_{PV}, x_{WT}, x_{ST}, x_{Battery}$, (ii) whether the ST collectors can export heat or not, y_{STConn} , or (iii) the main heat
 214 supply component, $y_{HeatSys}$.

215 **3.2. Objective functions**

216 The objective functions in this study are the annual operational equivalent CO₂ emissions of the system,
 217 and its LCC. For simplicity, the annual operational equivalent CO₂ emissions are henceforth referred to
 218 simply as CO₂ emissions.

219 The CO₂ emissions $CO_{2,eq}$ in kgCO₂eq/(m² a) are calculated as

$$CO_{2,eq} = \frac{(El_{imp} - El_{exp}) \cdot f_{CO_2,EL} + E_{NG} \cdot f_{CO_2,NG} + E_{WP} \cdot f_{CO_2,WP} - Q_{exp} \cdot f_{CO_2,off}}{A_{net}}, \quad (3)$$

220 where El_{imp} and El_{exp} are the annual electricity import and export respectively, E_{NG} and E_{WP} are the NG
 221 and WP energy demand respectively, Q_{exp} is the exported heat and $f_{CO_2,EL}$, $f_{CO_2,NG}$, and $f_{CO_2,WP}$ are the

222 specific emissions factors for electricity, NG and WP respectively. $f_{CO_2,off}$ is the specific emissions factor
223 for emissions reduction by heat export, which is calculated independently for each case study.

224 The LCC of the system is calculated as

$$LCC = I_{ini} + C_{O\&M} + C_{single} + C_E + A_{salv}, \quad (4)$$

225 where the net present value (NPV) of operational cash flows and salvage values are considered. I_{ini}
226 represents the initial investment including component prices, installation costs and connection costs, $C_{O\&M}$
227 represents the discounted operation and maintenance (O&M) costs of the system components, C_{single}
228 represents the discounted single entry expenses that occur every few years, such as component
229 replacements, C_E represents the discounted cash flow due to energy and/or fuel purchases and sales along
230 with any service fees that may apply, and A_{salv} represents the discounted salvage value of the components
231 that can be sold at the end of the lifetime considered in this study. To account for the price development of
232 the energy carriers, the NPV calculation of C_E uses a real interest rate that reflects price escalation rates. To
233 focus on the influence of the design variables, and for ease of interpretation, a differential lifecycle cost
234 ΔLCC is used, which is the difference between each case—with different values for the design variables—
235 and the reference case—which represents the most common energy supply method in each country; the
236 latter is defined independently for each case study.

237 **3.3. Design variables**

238 The design variables in this study represent the options for onsite heat and electricity generation, storage
239 and exchange. They address the installed capacity of PV, WT and ST collectors, the battery size, ability of
240 the ST collectors to export heat, and the main heat supply component. The maximum size of the PV system
241 has been defined based on the rooftop area of the reference buildings; a comparable size for the WT system
242 has been defined. The lower limit for the battery state of charge is 30%. The particular characteristics of
243 the variables are shown in Table 4 and Table 5. One multiobjective optimization process is performed for
244 each tag value of variable $y_{HeatSys}$; this allows finding the optimal results for each heating system and
245 prevents loss of information, thus overall offering a better basis for the analysis and comparison of the
246 results. Moreover, since the tag values represent different components rather than more typical increasing
247 or decreasing values, running a single optimization for all tags of $y_{HeatSys}$ is detrimental to the quality of
248 the results.

249

Table 4 – *Design variables in the optimization.*

250

Table 5 – *Features of the design variable for the main heat supply component $\mathbf{y}_{HeatSys}$.*

251 The installed capacity of GSHP and ASHP depends on the export capability: if heat export is not allowed
252 the installed capacity is 6 kW, whereas if heat export is allowed the installed capacity is 8 kW (see Table
253 5). This approach is taken based on Manrique Delgado et al. [17], where the results indicated that a higher
254 installed capacity is preferred when heat export is allowed.

255 In order to ensure that heat export by the ST collectors, GSHP or ASHP has no negative impact on the
256 energy supply of the building, the following rules have been implemented:

- 257 - The ST system can export heat only if the temperature in the bottom of the HWST is 60 °C or
258 higher.
- 259 - The GSHP and ASHP can export heat only if the electricity demand of the building is covered (i.e.
260 the GSHP or ASHP are operated with surplus electricity), the heat demand of the building is
261 covered (satisfying the heat demand of the building has priority over heat export), and the battery
262 is fully charged.

263

3.4. Simulation and multiobjective optimization

264 The building and energy systems have been modeled in TRNSYS 17, a simulation environment for transient
265 systems [43]. The simulation corresponds to one year of operation, with a time-step of 0.25 hours. The
266 model includes a network comprising the energy generation, storage and demand components, the
267 connections between them, the weather processors and the required control systems. Moreover, the
268 calculation of the objective functions takes place within the model, not during post-process. The weather
269 input for the Netherlands is based on the typical climate reference year NEN 5060:2008, which is based on
270 the average months of 20 years of historical data [46]. The weather input for Finland is based on the test
271 reference year TRY2012 [24].

272 The optimization process was performed in MOBO, a tool for multiobjective building performance
273 optimization [47, 48]. The optimization algorithm Pareto archive NSGA-II has been chosen from the
274 algorithm library available in MOBO. NSGA-II stands for *Nondominated Sorting Genetic Algorithm II*, an
275 evolutionary algorithm developed by Deb et al. [49]. As recommended by Alajmi et al. [50], the population
276 size is small, the crossover probability is high and the mutation rate is low, with values of 8, 100% and
277 20%, respectively. To find out the number of generations needed to find the optimal (or near-optimal)
278 solutions, a pre-optimization process with 100 generations was conducted and the number of generations
279 after which the Pareto front no longer showed a significant improvement was found. Further information
280 about this procedure is given in [17]. The number of generations was set at 45, for a total of 360 simulations

281 per case study. Different values in the variables, particularly in variable $y_{HeatSys}$, lead to different
282 simulation times and subsequently to different optimization times. A defined optimization time can thus
283 not be given, only an approximate of roughly 1.5 to 2 days of calculation time per optimization, for a total
284 of 20 to 22 days for the entire set of optimizations. A flow diagram of the simulation and optimization
285 process is shown in Figure 2. Both the TRNSYS model and the optimization have been implemented with
286 standard and/or available components and tools (e.g. Type94b for PV, Type1a for ST). Therefore, the
287 method used in this study can be replicated through the use of similar dynamic simulation environments
288 and optimization tools.

289 **Figure 2** – The flow diagram of the simulation and optimization process.

290 **4. Results & discussion**

291 In this section, the results of the multiobjective optimizations are presented and discussed. First, those
292 related to the Netherlands, followed by those related to Finland; the section closes with a comparison
293 between the two countries.

294 **4.1. The Netherlands**

295 The Pareto fronts for the three heating systems for the Dutch case with and without net-metering are shown
296 in Figure 3. The reference case consists of a system with an NG boiler, a connection to the electricity grid,
297 and no other heat or electricity generation components. The results show that ASHPs offer the optimal
298 solutions under both net-metering options, provided that there is a provision for heat export. This is
299 attributed to the higher monetary income from exported heat, of €0.13, than from exported electricity
300 (assuming an annual surplus), of €0.07. In case of net-metering, NG boilers have a lower ΔLCC compared
301 to ASHPs without heat export due to the lower investment cost of boilers. However, as more onsite
302 generation capacity is available, the optimal option between an NG boiler and an ASHP without heat export
303 depends on net-metering: if net-metering is available, ASHP is preferred in most of the front, whereas if
304 net-metering is not available, ASHP and NG boiler compete closely along the front. This is because an
305 ASHP benefits more from net-metering—an electricity oriented support scheme—than an NG boiler.

306 An ASHP with heat export has the lowest ΔLCC with net-metering compared to other heating systems: €
307 69.70/m² with CO₂ emissions of -41.1 kgCO₂eq/(m² a), yet increases to €4.0/m² without net-metering, with
308 no significant change in CO₂ emissions. This is attributed to heat export, which allows reduction of CO₂
309 emissions irrespective of net-metering. In cases of no heat export, the ΔLCC of an ASHP increases to €
310 17.5/m², and CO₂ emissions increase to -26.6 kgCO₂eq/(m² a) with net-metering, and to €1.1/m² and CO₂
311 emissions of -15.2 kgCO₂eq/(m² a) without net-metering. It is worth noting that the LCC is higher in cases
312 of no net-metering due to the lower income from exported electricity. Overall, an ASHP with heat export

313 is the optimal heating system with and without net metering. A natural gas boiler should be preferred if the
314 Δ LCC is prioritized and heat export is not allowed. A detailed investigation on the cost-optimal systems is
315 shown in Appendix B.

316 It can be observed from Figure 4 that the capacities for PV have similar trends for the three heating systems
317 with and without net-metering. The same observations can be made for WTs. Scattered capacities are
318 observed for ST and battery for both net metering options.

319 **Figure 3** – *The Pareto fronts for ASHP with and without heat export, and for boiler. The fronts are shown*
320 *for the Dutch case with (top) and without (bottom) net-metering.*

321 The difference in PV system capacities on the Pareto fronts with and without net-metering is not significant,
322 the only differences being the optimal capacity of a PV system for an ASHP with no heat export and for a
323 boiler in case of no net-metering. Cost optimality is lessened if there is no net-metering, as the excess
324 exported electricity yields lower benefits at the same investments costs. If heat export is allowed, higher
325 capacities of PV system yield optimal investment options as excess electricity generated by a PV system
326 can be utilized by the ASHP to generate heat. Overall, the optimal capacity of a PV system for the three
327 heating systems is between 9 to 10 kW, with a few solutions between 8 to 9 kW. An investigation on larger
328 installed capacities of PV can be found in Appendix B.

329 In contrast to the optimal capacities of PV systems, the trends for the optimal capacity of WTs cover the
330 entire range for the three heating systems with and without net-metering. There is no observable influence
331 of availability of net-metering on the overall investment strategy in WTs. WTs offer better energy matching
332 than PV systems due to their more evenly distributed energy generation throughout the days and the
333 seasons; this allows a higher rate of self-consumption, which reduces the export of surplus electricity and
334 thus the effect of net-metering.

335 Even though there is no definite trend for a ST collector area on the fronts, it can be observed from Figure
336 4 that higher capacities of ST systems dominate the Pareto front of ASHPs with and without export when
337 net-metering is available, and lower capacities otherwise. However, for the boiler, the capacities of ST
338 systems remain mostly unchanged on an average of 7 m²e. This indicates that heat generated by a ST system
339 can enhance the performance of ASHPs by (a) reducing the need to operate the ASHP to cover heat demand
340 by the building, and by (b) allowing the ASHP to export more heat. This second point is because PV and
341 ST generation are dependent on solar radiation; when the sun is shining, the ASHP, driven by surplus
342 electricity, can focus more on heat export since the ST collectors assist to cover the building heat demand.

343 Similar to the ST capacities on the fronts, scattered values for battery size are observed for the three heating
344 systems, yet the effect of net-metering is clearly visible: the average battery capacities for ASHP with heat

345 export are 1.8 kWh with net-metering and 3.6 kWh without net-metering. This is attributed to the grid
346 acting as virtual storage in case of net-metering. The installed battery capacities for an ASHP without heat
347 export and an NG boiler are similar for both net-metering options, with scattered values across the whole
348 front. While this could seem counter intuitive, it is an indication that the battery size has little influence on
349 the results, and the optimization algorithm prioritizes exploring other variables.

350 **Figure 4** – *Installed capacity of onsite generation and storage components on the optimal fronts for an*
351 *ASHP with and without heat export, and for a natural gas boiler. Capacities are shown for the Dutch*
352 *case with (left) and without (right) net-metering.*

353 **4.2. Finland**

354 Figure 5 shows the Pareto fronts for the three main heat supply components, for the Finnish cases with and
355 without net-metering. The reference case consists of a system that covers its heating and electricity demands
356 through imports from the district heating and electricity grids. The results of the multiobjective optimization
357 show that GSHPs offer the optimal solutions for LCCs and CO₂ emissions. As for comparing between
358 GSHPs with and without heat export, the results without net-metering show that the lowest Δ LCC, €
359 46.5/m², is reached when the GSHP cannot export heat. For comparison, the lowest Δ LCC for a GSHP with
360 export is €24.5/m². Yet, while there is an increase in the LCC, the system with heat export allows a
361 significant reduction of 20.2 kgCO₂eq/(m² a), offering a net compensation of CO₂ emissions. If net-metering
362 is available, the lowest LCC for GSHPs without and with heat export drop to €84.2/m² and €65.6/m²,
363 respectively. Otherwise, there are no major differences between the cases with and without net-metering
364 (see Figure 5).

365 As in the Dutch case, the dominance of heat pumps on the Pareto front relies on the COP of this component.
366 Let us assume there is 1 kWh of surplus electricity generated by the PV system. If it were directly exported
367 to the Finnish grid, it would compensate 0.173 kgCO₂eq, and the income from its sale would be roughly
368 €0.03. Yet, if it were converted to heat and exported to the heating grid, it would compensate 0.857
369 kgCO₂eq, and the income from its sale would be roughly €0.13. That is, by converting 1 kWh to heat for
370 export, the system compensates 4.9 times more emissions and brings 4.3 times more income. Regarding
371 the LCC difference between the GSHP with and without heat export, the heat export option dominates the
372 top part of the front due to the higher monetary income from exported heat, while the electricity export
373 option dominates the bottom part due to its lower initial investment. Moreover, the presence on the optimal
374 front of GSHPs with export indicates that the income from heat export can justify the additional spending
375 on borehole depth and connection costs if onsite electricity generation is available and sizable.

376

377 **Figure 5** – *The Pareto fronts for GSHPs with and without heat export, and for boilers. The fronts are*
378 *shown for the Finnish case without (top) and with (bottom) net-metering.*

379 It can be observed from Figure 6 that with net-metering the optimal results have at least 6-kW PV capacity,
380 regardless of the main heat supply component, whereas without net metering several systems with lower
381 PV capacity are present on the optimal fronts of GSHPs without export and boilers. The lower PV capacities
382 when net-metering is not available reinforce the notion that net-metering has a positive effect on the
383 economic performance of PV systems. An investigation on larger installed capacities of PV can be found
384 in Appendix B. Regarding batteries, Figure 6 shows that there is no clear pattern when the system includes
385 a boiler or a GSHP without heat export. However, if a GSHP with export is present, the battery size should
386 be below 3 kWh.

387 **Figure 6** – *Installed capacity of onsite generation and storage components on the optimal fronts for*
388 *GSHPs with and without heat export, and for boilers. Capacities are shown for the Finnish case with*
389 *(left) and without (right) net-metering.*

390 These results indicate that investments in onsite electricity generation components should be first directed
391 to the PV system, followed by WTs. The results are not as conclusive regarding whether investments in ST
392 collectors or WTs are preferred, since they seem to be related to the main heat supply component. For
393 GSHPs without heat export and boilers, the investments in ST collectors along the Pareto front are
394 concentrated mostly between 8 and 10 m², whereas for GSHPs with export the investments are concentrated
395 mostly between 0 and 2 m². Particularly, when a GSHP is allowed to export investing in WTs is more
396 attractive than investing in ST collectors, since more surplus electricity by WTs (to generate and export
397 heat) brings higher income than more surplus heat by the ST collectors. In contrast, when a GSHP is not
398 allowed to export, WTs and ST collectors compete more closely, and thus investment in both is significant.

399 The availability of net-metering is shown to have limited effects on the behaviour of the optimal fronts and
400 component investments. It is remarkable that batteries do not show a defined trend when a boiler or GSHP
401 without export are present. This could be due to their relatively scarce effect on the results, since batteries
402 have relatively lower prices and lower overall influence on the system compared to PV, WT and ST
403 collectors. Yet, if a GSHP with export is present, the battery size should be kept low so as to promote heat
404 export, which explains the distribution seen in Figure 6.

405 **4.3. Similarities and contrasts**

406 A significant difference is that the environmental attractiveness of converting surplus electricity into heat
407 for export is lower in the Netherlands than it is in Finland, due to the high emission factor of electricity in
408 the Netherlands. For instance, if 1 kWh of surplus electricity is exported to the grid, it compensates 0.540

409 kgCO₂eq, while if it were converted to heat and exported to replace heat from an NG boiler, it would
410 compensate 0.969 kgCO₂eq. Thus, converting 1 kWh to heat the system compensates roughly 1.8 times
411 more emissions. While this is attractive, in Finland the ratio is considerably higher, at 4.9.

412 Moreover, the climatic differences between the Netherlands and Finland have notable impacts on onsite
413 energy generation. The higher solar radiation in the Netherlands means a higher output per unit of installed
414 capacity than in Finland. As an example, a 1-kW PV system delivers 1,111 kWh/a of electricity in the
415 Netherlands but only 907 kWh/a in Finland. This, in combination with the different export price schemes,
416 could translate into an income of €77.8 in the Netherlands and €29.0 in Finland, assuming all the generation
417 is exported as surplus, or into annual savings of €22.0 in the Netherlands and €139.0 in Finland, assuming
418 all the generation is used onsite.

419 *4.3.1. Heating systems*

420 The results of the multiobjective optimizations of heating systems for the Dutch case (Figure 3) and the
421 Finnish case (Figure 5) show that heat pumps offer the optimal solutions for LCCs and CO₂ emissions with
422 and without net-metering. However, if heat export is not available, the NG boiler has the lowest LCC in the
423 Dutch case regardless of whether net-metering is available or not. This is attributed to the lower initial
424 investment of NG boilers in the Netherlands. Notably, it is found that ASHPs and GSHPs with heat export
425 result in the lowest CO₂ emissions for both net-metering options.

426 A reason for the differences between the Dutch and Finnish contexts is the type of heat pumps. In the
427 Netherlands, ASHPs are more common, as winters are milder and the component can offer a satisfactory
428 performance throughout the year. This is not the case in Finland, where outdoor temperatures during winter
429 are lower and ASHP performance is drastically diminished. GSHPs are more common in Finland, as the
430 ground temperature is not as low as the ambient air temperature, which subsequently helps the COP to
431 remain acceptable.

432 *4.3.2. Fluctuating generation components*

433 High capacities of PV systems—between 9 to 10 kW for the Dutch case and between 6 to 10 kW for the
434 Finnish case—are found to be optimal irrespective of heating system type in the case of net-metering.
435 However, in the case of no net-metering, this optimal capacity lower limit reduces for ASHPs with no heat
436 export to 8 kW in the Dutch case. This reduction is even greater in the Finnish case—it is close to zero for
437 GSHPs with no heat export. The optimal capacity of a WT system varies from 0 to 10 kW for both the
438 Dutch and Finnish cases for all heating systems and net-metering options. Overall, the behaviour of
439 investments in WT systems shows no significant differences between countries.

440 ST collectors show more distinct differences between the Dutch and Finnish cases. However, in the Finnish
441 case, the investments in ST collectors are rather polarized They tend to be low for GSHPs with export, yet
442 high for the two other heat supply systems, whereas in the Dutch case, the investments on ST collectors are
443 quite scattered and thus less conclusive.

444 *4.3.3. Electricity storage component*

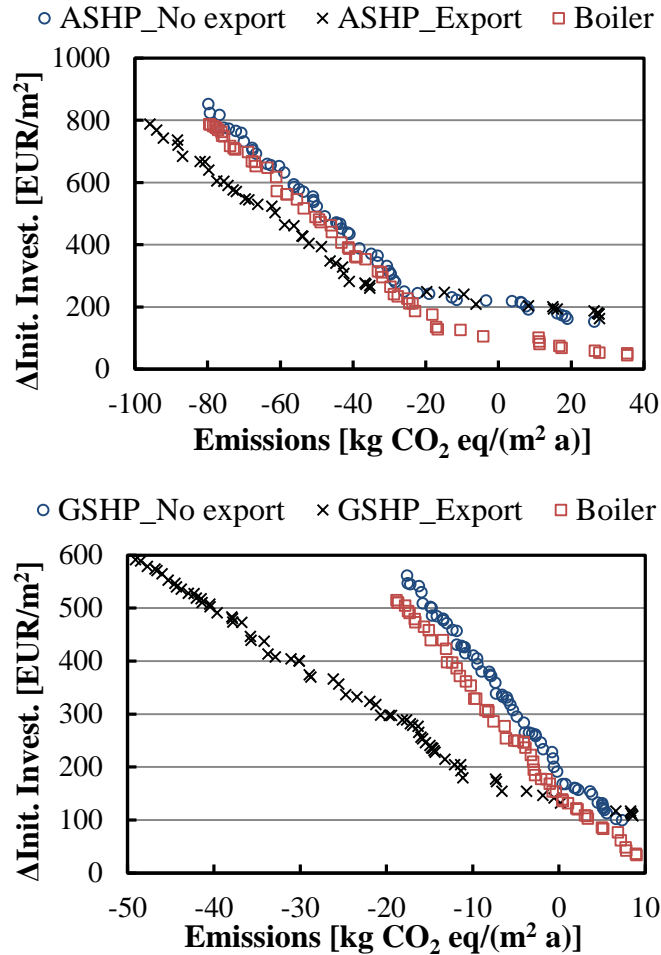
445 The availability of net-metering is shown to have limited effect on the behaviour of the investments on
446 electricity storage components in the Dutch and the Finnish cases, with average installed capacities of 3.6
447 and 2.8 kWh, respectively. Thus, this component does not seem to have a strong impact on the system
448 performance of the studied cases, with the only remarkable effect of net-metering being shown in ASHP
449 with heat export in Netherlands.

450 *4.4. Initial investment subcase*

451 A supplementary set of multiobjective optimizations was conducted for both countries: CO₂ emissions and
452 initial investment. This subcase allows studying the heat export strategy from the perspective of a
453 contractor, who pays the initial cost yet does not benefit from savings. The results are shown in Figure 7.
454 Net-metering has no effect in these optimizations; therefore, only one set of results is presented.

455 Boilers provide optimal solutions with low initial investment in both countries. This is a consequence of
456 the lower price of boilers compared to ASHP and GSHP, and of the lower specific emissions factor of NG
457 and WP compared to the specific emissions factors of electricity in the Netherlands and Finland,
458 respectively. These factors also explain the steep decrease in the lower part of the fronts: as investment in
459 onsite electricity generation components increases, the CO₂ emissions caused by electricity imports
460 decrease sharply. As the initial investment increases, surplus electricity from onsite generation components
461 becomes available for generating and exporting heat, thus allowing heat pumps with heat export capability
462 to become optimal solutions in both countries.

463 The Pareto fronts in the Finnish case shows that, except for systems with little to no investment on onsite
464 generation components, the results for GSHP with heat export dominate those for GSHP without export.
465 This is a consequence of the COP and of higher specific emissions factor of DH compared to that of
466 electricity: not only can more units of heat than of electricity be exported, but each unit offsets of heat
467 offsets more CO₂ emissions. In contrast, the high specific emissions factor of electricity in the Netherlands
468 causes both options of ASHP to compete closely in the lower portion of the fronts: only when the size of
469 PV system reaches roughly 7 kW does ASHP with heat export become the identifiable optimal solution.



470

471

472 **Figure 7** – The Pareto fronts of the multiobjective optimization for CO₂ emissions and initial investment.
 473 The fronts are shown for the Dutch case (top) and the Finnish case (bottom).

474 The results of this subcase show conflictive preferences at low investments: the optimal solutions for a
 475 contractor require a boiler while the optimal solutions for an end user require a heat pump. In an ideal
 476 situation, an informed end user would cover the higher initial investments knowing that the savings will
 477 exceed the costs, yet other users might prioritize low initial costs. Moreover, a contractor might prefer
 478 solutions with a low initial cost as they can be afforded by a larger portion of the population. Therefore,
 479 understanding of the immediate and long-term economical advantages of the system is necessary to ensure
 480 that the energy system is optimal—or close to optimal—for both parties.

481 **4.5. Uncertainty analysis**

482 An uncertainty analysis was conducted to address the influence of changes in the economic context. Two
 483 economic parameters were investigated: the energy price escalation rates and the heat export price. The
 484 energy price escalation rates are set at 0% and 2%, while the heat export price are set as 30% and 50%. An

485 uncertainty analysis for the Finnish case is not presented in this study, as it has been addressed by Manrique
486 Delgado et al. [17] for a similar optimization problem.

487 Figure 8 shows non-dominated fronts for CO₂ emissions and the ΔLCC for the optimizations with 0%, 1%
488 and 2% energy price escalation rates. The results for all systems show similar behaviour: higher escalation
489 rates lead to lower ΔLCC, because higher escalation rates mean higher income from energy export in the
490 future. The difference in LCC caused by the escalation rates is more pronounced at high values of ΔLCC.
491 This difference can be explained by the investments in onsite generation: as investments increase, energy
492 export increase, and thus the energy price escalation rates have a stronger effect on the LCC. Regarding the
493 investments in PV, WT, ST collectors and battery capacity, there are no remarkable differences compared
494 to the optimization with the calculated energy price escalation rates.

495 Figure 9 shows the non-dominated fronts for ΔLCC and CO₂ emissions for the optimizations with a heat
496 export price at 30%, 40% and 50% of the retail price. It can be seen that lower export prices lead to higher
497 LCCs. This is a consequence of the income from heat export: the higher the export price, the higher the
498 income. Further, it can be seen that at the top of the figure the difference between ΔLCCs can reach €119/m²
499 for similar emission levels, whereas at the bottom it decreases to €36/m². The reason for this difference in
500 ΔLCC is the amount of exported heat. The influence of the export price of heat increases along the front,
501 simply because there is more heat to export. Regarding the investments in PV, WT, ST collectors and
502 battery capacity, there are no remarkable differences compared to the optimization with 40% of the retail
503 price.

504 Overall, the results of the uncertainty analysis show that the main findings discussed above remain valid
505 under the tested conditions. That is, the LCCs of the systems investigated are influenced by the escalation
506 rates and by the heat export prices, yet there is no notable change in the observation that ASHPs with heat
507 export offer the lowest ΔLCCs and a significantly higher compensation of CO₂ emissions. Moreover, the
508 observation that the optimal front for ASHPs with heat export dominates the optimal front for ASHPs
509 without heat export remains valid. Regarding the investment in other components such as PV or WT
510 systems, no significant changes were observed.

511 **Figure 8** – *The non-dominated fronts for an ASHP without export (top), an ASHP with export (bottom*
512 *left) and (bottom right), with calculated (1%), low (0%) and high (2%) energy price escalation rates.*

513 **Figure 9** – *The non-dominated fronts for an ASHP with export at different heat export prices, shown as a*
514 *percentage of the retail price, and for an ASHP without export and boiler.*

515 **5. Conclusions**

516 This study consists of multiobjective optimizations for CO₂ emissions and LCCs of residential-scale energy
517 systems with onsite electricity and heat generation components. Moreover, two different energetic,
518 economic and climatic contexts were explored: the Netherlands and Finland. The main outcomes of the
519 study are as follows:

- 520 • Heat pumps represent the optimal main heat supply component in the Netherlands and Finland, and
521 the PV system is the most attractive supplementary onsite generation component followed by WTs.
- 522 • The environmental attractiveness of converting surplus electricity into heat for export is lower in
523 the Netherlands than in Finland due to the CO₂ emission factors.
- 524 • The calculated optimal investments in the PV system in the Netherlands start at 8 kW without net-
525 metering and at 9 kW with net-metering, whereas in Finland, the calculated optimal investments in
526 the PV system start at 6 and 0 kW, respectively. However, the maximum optimal PV capacity
527 would likely require an area that exceeds the typical rooftop area of a single family building.
- 528 • Overall, investments in PV systems should be preferred over investments in WT systems, with no
529 significant differences based on the country.
- 530 • Energy systems, where surplus electricity is used to drive an ASHP and export heat, leads to optimal
531 solutions for CO₂ emissions and Δ LCCs in the Netherlands, with calculated values of -41.1
532 kgCO₂eq/(m² a) and €69.7/m² for the cost-optimal solution.
- 533 • Net-metering allows reducing the calculated Δ LCC of the energy system by 65.7/m² in the
534 Netherlands. The availability of net-metering does not affect the performance ranking of the studied
535 heat and electricity systems, and no significant differences arise in the energy system configuration
536 if net-metering is present or not.
- 537 • The results of the uncertainty analysis to energy price escalation rates and heat export prices in the
538 Netherlands show that the performance ranking of the studied heat and electricity systems remain
539 valid under the tested conditions.
- 540 • Energy systems consisting of a GSHP with and without the ability to export heat lead to optimal
541 solutions for CO₂ emissions and Δ LCCs in Finland, with calculated values of 8.9 kgCO₂eq/(m² a)
542 and €46.50/m² for the cost-optimal solution. The Pareto front consists of systems including a
543 GSHP with the ability to export surplus heat, except in its bottom part, which consists of systems
544 without this ability.
- 545 • Net-metering allows reducing the calculated Δ LCC of the energy system by €41.0/m² in Finland.
546 As in the Netherlands case, the availability of net-metering does not affect the performance ranking
547 of the studied heat and electricity systems, and no significant differences arise in the energy system
548 configuration if net-metering is present or not.

549 • Boilers are the optimal main heat supply components for systems with low initial investments,
550 whereas heat pumps are optimal for systems with low LCC. This may create a conflict of interests
551 between the investor and the end user.

552 The outcomes rely on the assumption that an unlimited amount of heat can be exported to the grid. While
553 this might seem counterintuitive, particularly during summer when heating demand is low, the assumption
554 is supported by the increasing interest in smart and efficient use of energy. Therefore, the exported heat
555 could be used in district cooling – through thermal cooling [51] – and/or in other thermally activated
556 technologies [52], seasonal storage, or to cover domestic hot water demand. Thus, as the energy systems
557 continue to develop, heat export to district grids has potential to become a common practice.

558 The contexts explored in this study give valuable insight into the potential of prosumers in central and
559 northern Europe, yet significant differences might arise in other geographical locations, indicating the need
560 for separate case study assessments. Furthermore, the support schemes to promote renewable energy
561 systems in single-family houses have a clear effect on the economic attractiveness of investing in such
562 components. Finally, the variable ranges should be adapted for each particular case, so as to find the optimal
563 energy system for the available conditions.

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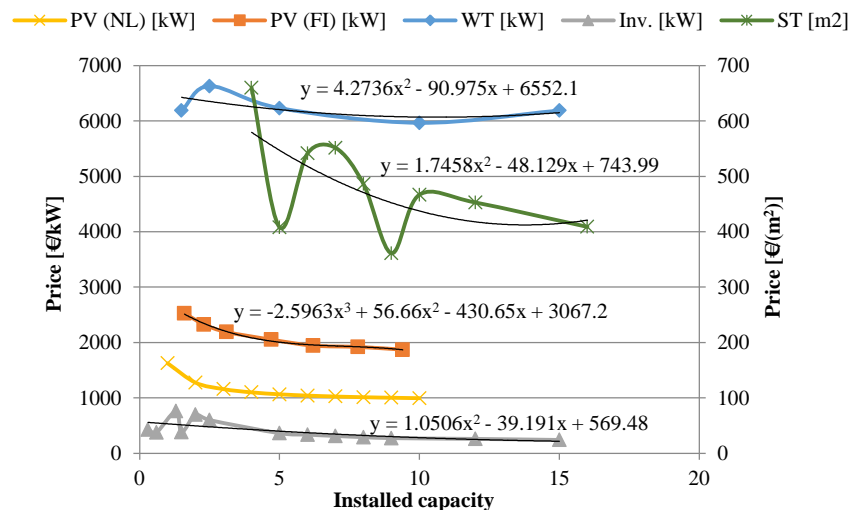
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574 Appendix A: Prices

575 Figure A shows the prices (including VAT) per installed capacity for several system components. PV prices
 576 in the Netherlands are calculated as $700+925*x$, where x represents the PV capacity in kW; the curve in the
 577 figure shows the price per installed capacity. All prices shown include installation costs, except for the ST
 578 collectors; for this component the installation costs are assumed to be equal to the price of the ST collectors.
 579 Battery prices are calculated as $192.09 x^{0.717}$, where x represents the battery size in kWh. Borehole and
 580 piping prices are calculated as €33.45/m of borehole depth and €15.00/m² of gross building area,
 581 respectively. The borehole depth was calculated using Earth Energy Designer [53] based on the onsite
 582 electricity generation capacity. Table A shows the annual O&M costs for PV, WT and ST components.
 583 Table B shows the lifespan of the components that require replacement. Table C shows the initial
 584 investment and O&M costs for the main heat supply components, and Table D shows the references for the
 585 initial investment and O&M costs.

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Figure A – Prices and price trends for system components.

589

Table A – Annual O&M costs as percentage of the initial investment for PV, WT and ST components.

Generation component	Annual O&M
PV	1%
WT	1.5%
ST	0.75%

590

Table B – Lifespan of system components that require replacement.

Component	Lifespan [years]
Inverter	12
Battery	10
ASHP/GSHP	20

591 Table C – Initial investment and O&M costs of the main heat supply components.

Heat supply component	Initial investment [€]	Annual O&M cost
GSHP – 6 kW	5300	1.5% of initial investment
GSHP – 8 kW	5500	1.5% of initial investment
ASHP – 6 kW	12,995	1.5% of initial investment
ASHP – 8 kW	13,545	1.5% of initial investment
Boiler – WP	3582	€139.2
Boiler – Gas	1099	€130.44

592

593 Table D – Sources for the initial investment and O&M costs of system components.

Component	Initial Investment		O&M	
	Source	URL	Source	URL
PV (NL)	Netherlands Enterprise Agency RVO, 2014	http://www.rvo.nl/onderwerpen/duurzaam-ondernemen/gebouwen/utliliteitsbouw/beheer-en-onderhoud/investeringskosten	National Renewable Energy Laboratory	nrel.gov/docs/fy15osti/63235.pdf
PV (FI)	Fortum	fortum.com		
WT	The Renewable Energy Hub UK	renewableenergyhub.co.uk	Wind Measurement International	windmeasurementinternational.com/wind-turbines/om-turbines.php
Inverter	Nettiosa	nettiosa.com	-	-
	Aurinko	aurinkosinoorit.fi		
	Finnwind	verkkokauppa.finnwind.fi		
ST	Ympäristöenergia	energiakauppa.com	National Renewable Energy Laboratory	nrel.gov/analysis/tech_cost_om_dg.html
	Sundial	sundial.fi		
	JTV-Energia	jtv-energia.fi		
Battery	Wholesale Solar	wholesalesolar.com/	-	-
Borehole and piping	Building Construction Cost Data 2013 [Talorakennuksen kustannustieto 2013]	-	-	-
GSHP – 6 kW	Taloon	taloon.com/ds/hakutulokset?q=nibe+1145	Mohamed, Hamdy, Sirén	dx.doi.org/10.1016/j.apenergy.2015.04.096
GSHP – 8 kW				
ASHP – 6 kW	Mitsubishi Electric	Direct quote	British Gas	britishgas.co.uk/home-services/home-cover/
ASHP – 8 kW				
Boiler – WP	National Renewable Energy Laboratory	nrel.gov/analysis/tech_cost_om_dg.html	British Gas	britishgas.co.uk/home-services/home-cover/
Boiler – Gas	Warmgarant	https://www.warmgarant.nl/cv-ketel-kopen/uw-cv-ketel-samenstellen/intergas-hreco-24.aspx	Warmgarant	https://www.warmgarant.nl/cv-ketel-kopen/uw-cv-ketel-samenstellen/intergas-hreco-24.aspx

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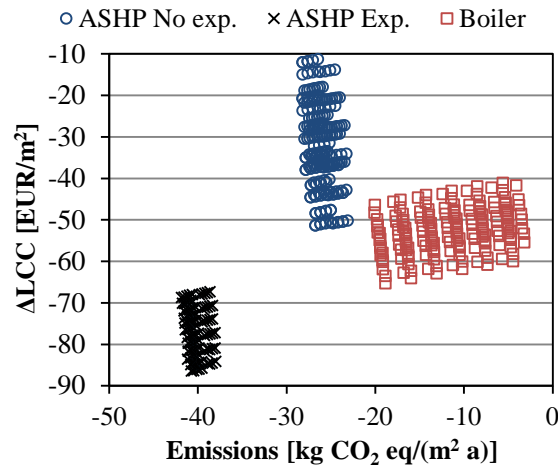
596 Appendix B: Complementary investigations

597 B.1: Cost-optimal systems verification

598 The optimization algorithm aims to cover most of the non-dominated front. Nevertheless, being a stochastic
599 algorithm, it might not succeed in finding the two optimal extreme solutions at the two ends of the Pareto
600 front. Since the minimum LCC point is the lower extreme point in the optimization search, therefore and
601 to ensure that the ASHP with heat export offers the solutions with lowest LCCs in the study case, a
602 supplementary set of simulations has been conducted. These optimizations use the exhaustive search
603 algorithm in MOBO (Brute-force search) with discrete variables. The insights about the upper and lower
604 limits and steps of the discrete variables are learned from the lowest-LCC results of the case study
605 optimization for each main heat supply system in Figure 3. The results of these supplementary simulations
606 are shown in Figure B.1, with a total of 469 simulations.

607 As can be seen in Figure B.1, the observation that ASHPs with heat export offer the lowest LCC is supported
608 by the explorative simulations. Moreover, a lower LCC solution has been found with €84.10/m² and CO₂
609 emissions of -38 kgCO₂eq/(m² a). These results support that the method allows the identification of the
610 main heat supply components that offer the lowest LCCs, yet they also remind us that solutions found by
611 stochastic optimization algorithms are near-optimal.

612



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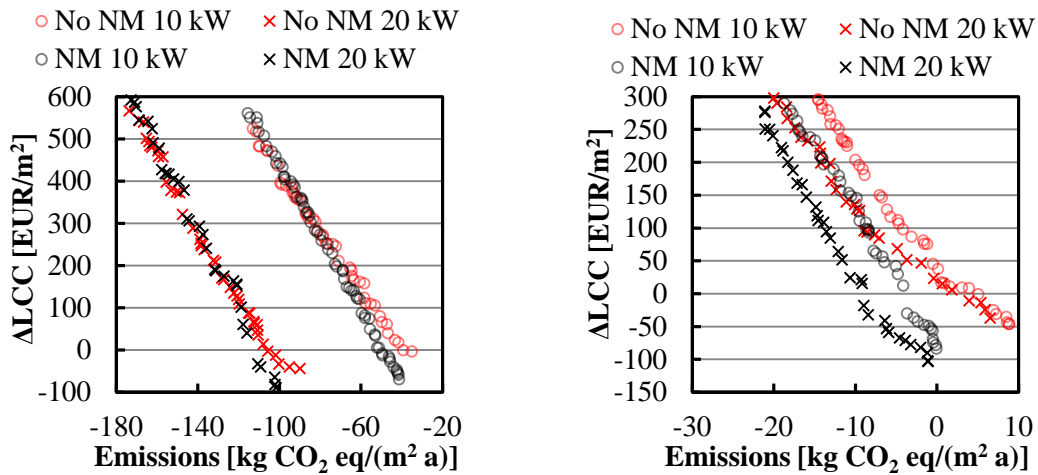
614 **Figure B.1** – The exploration of the lowest LCC systems on the fronts in the Dutch case with net-
615 metering.

616 B.2: Saturation of PV

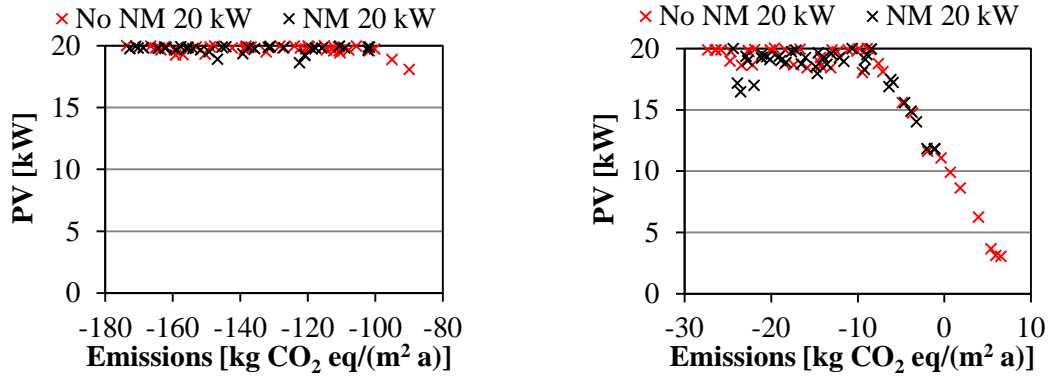
617 Figures 4 and 6 show that investments in PV systems reach the maximum defined in this study in several
618 cases. Thus, extended optimizations for the Netherlands and Finland have been conducted to investigate if

619 larger PV systems would provide optimal solutions; the results of the previous and the extended
 620 optimizations for the Netherlands and Finland can be seen in Figure B.2. The maximum PV capacity has
 621 been increased to 20 kW, while the ranges for the rest of the variables remain unchanged; Figure B.3 shows
 622 the installed capacity of PV on the optimal fronts. Moreover, only the system with the lowest LCC is
 623 included, namely the ASHP system with heat export in the Netherlands and the GSHP system without heat
 624 export in Finland.

625 The results provide two remarkable outcomes. First, the optimal PV capacity does not lie within the 10-kW
 626 range given in this study, as the Pareto fronts from the 10-kW optimizations are dominated by the fronts of
 627 the 20-kW optimizations in all the explored cases. However, it must be underlined that single-family
 628 buildings usually have limited rooftop area, and thus installing large PV systems may be unfeasible; this is
 629 the case in the studied buildings. Second, systems with a LCC lower than in the previous optimizations
 630 were found for each case. This implies that the LCC optimum lied outside the variable ranges investigated
 631 in this study, and potentially lies even outside the extended PV range. These two outcomes reinforce the
 632 need to search for the optimal energy system based on the conditions particular to each building, such as
 633 available rooftop area and energy demand.



634
 635 **Figure B.2** – The extended optimization with up to 20-kW PV for ASHP with export in Netherlands (left),
 636 and the extended optimization with up to 20-kW PV for GSHP without heat export in Finland (right), with
 637 (NM) and without (No NM) net-metering.



638

639 **Figure B.3** – *The installed capacity of PV on the optimal front in extended optimization with up to 20-kW*
 640 *PV for ASHP with export in Netherlands (left), and the installed capacity of PV on the optimal front in the*
 641 *extended optimization with up to 20-kW PV for GSHP without heat export in Finland (right), with (NM)*
 642 *and without (No NM) net-metering.*

643

644